

Example Problem 7.1

Given: The following members are being considered for use as a concentrically loaded column. The column has effective lengths, KL , of 15 ft in one direction and 6 ft in the orthogonal direction. The load consists of 1 part Dead Load, 1.5 parts Live Load and 2 parts Snow Load.

- a) W10x19
- b) Rectangular HSS 10x4x1/2
- c) Round HSS 7.5x0.500

Wanted: Determine the capacity of each section for each condition. Consider both ASD and LRFD, expressing the results in comparable terms.

Solution:

NOTE: IT IS BEST TO ORIENT THE STRONG AXIS OF THE COLUMN WITH THE LONGEST KL .

COMPUTE COMPOSITE LOAD FACTORS

LRFD: LC-3a CONTROLS (VERIFY THIS!)

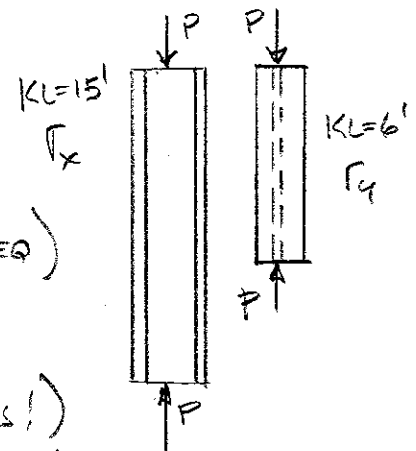
$$P_u = 1.2 \left(\frac{1}{4.5} P_{s,eq} \right) + 1.6 \left(\frac{2}{4.5} P_{s,eq} \right) + 1 \left(\frac{1.5}{4.5} P_{s,eq} \right)$$

$$P_u = \underline{\underline{1.31 P_{s,eq}}}$$

ASD: LC-4 & LC-6 CONTROLLED EQUALLY (VERIFY THIS!)

$$P_a = 1 \left(\frac{1}{4.5} P_{s,eq} \right) + .75 \left(\frac{1.5}{4.5} P_{s,eq} \right) + .75 \left(\frac{2}{4.5} P_{s,eq} \right)$$

$$P_a = \underline{\underline{0.806 P_{s,eq}}}$$



PART (a) CHECK LOCAL BUCKLING (SCM TABLE B4.1)

$$\text{CASE 3: } \frac{b_f}{2t_f} = 5.09 \leq .56 \sqrt{\frac{29,000 \text{ ksi}}{50 \text{ ksi}}} = 13.5 \therefore \text{NOT SLENDER}$$

$$\text{CASE 10: } \lambda_{cW} = 35.4 \leq 1.49 \sqrt{\frac{29,000 \text{ ksi}}{50 \text{ ksi}}} = 35.9 \therefore \text{NOT SLENDER}$$

SECTION IS NOT SLENDER $\therefore Q = 1$

USE EITHER SCM E2 OR E7
 $\uparrow$ USE

PROBLEM 7.1 (CONTINUED)

ZBQ = 4

$$\text{SLENDERNESS: } \left(\frac{KL}{r}\right)_x = \frac{15'(12"/ft)}{4.14"} = 43.5$$

$$\left(\frac{KL}{r}\right)_y = \frac{6'(12"/ft)}{1.874"} = 82.4 \leftarrow \text{GOVERNS}$$

DETERMINE F_{cr} & P_n

$$\frac{KL}{r} = 82.4 \leq 4.71 \sqrt{\frac{E(29,000 \text{ ksi})}{50 \text{ ksi}}} = 113.4 \therefore \text{USE SCM EQ E3-2}$$

$$F_e = \frac{\pi^2(29,000 \text{ ksi})}{(82.4)^2} = 42.2 \text{ ksi}$$

$$F_{cr} = [0.658^{(50/42.2)}] (50 \text{ ksi}) = 30.4 \text{ ksi}$$

$$P_n = (30.4 \text{ ksi})(5.62 \text{ in}^2) = 171.1 \text{ k}$$

LRFD: $\phi = 0.9$; $P_u = 1.31 P_{s,eq} \leq 0.9 (171.1 \text{ k}) = 154.0 \text{ k}$

$$P_{s,eq} \leq 117.4 \text{ k} \leftarrow \text{ANSWER (a)}$$

ASD: $\Omega = 1.67$; $P_a = 0.806 P_{s,eq} \leq 171.1 \text{ k} / 1.67 = 102.4 \text{ k}$

$$P_{s,eq} = 127.2 \text{ k} \leftarrow \text{ANSWER (a)}$$

PART (b): CHECK LOCAL BUCKLING (DIFFERENT THAN W SECTION!)

CASE 12: $b/t = 18.5 \nless 1.40 \sqrt{\frac{29,000 \text{ ksi}}{46 \text{ ksi}}} = 14.06 \therefore \text{SLENDER}$

$$b_e = 1.92(0.465") \sqrt{\frac{29,000}{46}} \left[1 - \frac{0.38}{18.5} \sqrt{\frac{29,000}{46}} \right] = 10.8" \text{ (EQ E7-18)}$$

$$b_e = 10.8" \nless b = (b/t)t = (18.5)(0.465") = 8.6" \therefore A_{eff} = A_g$$

$$\left. \begin{matrix} Q_a = 1 \\ Q_s = 1 \end{matrix} \right\} Q = Q_s Q_a = 1.0 \therefore \text{LOCAL BUCKLING HAS NO EFFECT IN THIS CASE}$$

SLENDERNESS

$$\left(\frac{KL}{r}\right)_x = \frac{15'(12"/ft)}{3.34"} = 53.9 \leftarrow \text{GOVERNS}$$

$$\left(\frac{KL}{r}\right)_y = \frac{6'(12"/ft)}{1.59"} = 45.3$$

PROBLEM 7.1 (CONTINUED)

DETERMINE SCM E7 EQUATION TO USE, F_{cr} , $\frac{1}{2} P_N$

$$\frac{KL}{r} = 53.9 \leq 4.71 \sqrt{\frac{29,000 \text{ ksi}}{(1)(46 \text{ ksi})}} = 118.2 \therefore \text{USE E7-2}$$

$$F_e = \frac{\pi^2 (29,000 \text{ ksi})}{(53.9)^2} = 98.6 \text{ ksi}$$

$$F_{cr} = (1) \left[.658^{\frac{(1)(46)}{98.6}} \right] (46 \text{ ksi}) = 37.8 \text{ ksi}$$

$$P_N = (37.8 \text{ ksi})(11.6 \text{ in}^2) = 439 \text{ K}$$

LRFD: $P_u = 1.31 P_{s,eq} \leq .9(439 \text{ K}) = 395 \text{ K}$

$$\boxed{P_{s,eq} \leq 301 \text{ K}} \leftarrow \text{ANSWER (b)}$$

ASD: $P_a = 0.806 P_{s,eq} \leq 439 \text{ K} / 1.67 = 263 \text{ K}$

$$\boxed{P_{s,eq} \leq 326 \text{ K}} \leftarrow \text{ANSWER (c)}$$

PART (c): CHECK LOCAL BUCKLING

CASE 15: $D/t = 16.1 \leq .11 \frac{29,000 \text{ ksi}}{42 \text{ ksi}} = 76.0 \therefore \text{NOT SLENDER}$

SLENDERNESS: $\left(\frac{KL}{r}\right)_x = \frac{15'(12"/ft)}{2.49"} = 72.3 \leftarrow \text{GOVERNS}$

$$\left(\frac{KL}{r}\right)_y = \frac{6'(12"/ft)}{2.49"} = 28.9$$

DETERMINE SCM EQ, F_{cr} , $\frac{1}{2} P_N$

$$KL/r = 72.3 \leq 4.71 \sqrt{\frac{29,000 \text{ ksi}}{42 \text{ ksi}}} = 123.8 \therefore \text{EQ E3-2}$$

$$F_e = \frac{\pi^2 (29,000 \text{ ksi})}{(72.3)^2} = 54.8 \text{ ksi}$$

$$F_{cr} = \left[.658^{\frac{42}{54.8}} \right] (42 \text{ ksi}) = 30.47 \text{ ksi}$$

$$P_N = (30.47 \text{ ksi})(10.3 \text{ in}^2) = 314 \text{ K}$$

PROBLEM 7.1 (CONTINUED)

LRFD: $P_u = 1.31 P_{s,eq} \leq .9 (314k) = 282k$

$$\boxed{P_{s,eq} \leq 215k} \leftarrow \text{ANSWER (c)}$$

ASD: $P_a = 0.806 P_{s,eq} \leq 314k / 1.67 = 188k$

$$\boxed{P_{s,eq} \leq 233k} \leftarrow \text{ANSWER (c)}$$

SOLUTION SUMMARY

PART	SECTION	STEEL	LRFD	ASD
(a)	W10x19	A992	117k	127k
(b)	HSS 10x4 x 1/2	A500, GRB, RECT	301k	326k
(c)	HSS 7.5 x 1/2	A500, GRB, RND	215k	233k

- TO SEE EFFECT OF GENERAL SLENDERNESS, EXPERIMENT WITH LOWER VALUES OF $(KL)_x$ & $(KL)_y$.
- EXPERIMENT WITH DIFFERENT SECTIONS, LOAD COMBINATIONS, AND LENGTHS TO GET A FEEL FOR THE BEHAVIOR OF THE EQUATIONS